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A DAMAGE ASSESSMENT MODEL FOR SURFACE ENGAGEMENT FOR MISSILE AN--ETC(U)

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NAVAL POSTGRADUATE SCHOOL
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THESIS

A Damage Assessment Model for Surface
Engagement for Missile and Gunfire

by

Mario Ivan Carratu Molina

March 1982

Thesis Advisor: Wayne P. Hughes, Jr.

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The hits on a target are assumed to be distributed uniformly along a target's length. Target elements (gun mounts, communications propulsion, etc.) are degraded or destroyed according to assigned vulnerability factors. To exercise the model, when experimental data was not available, judgmental inputs were used. The resulting outputs were realistic. The model uses a computer program written in Fortran four with Montecarlo features incorporated.



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A DAMAGE ASSESSMENT MODEL FOR SURFACE ENGAGEMENT FOR MISSILE
AND GUNFIRE

BY

MARIO IVAN CARPATHI MOLINA
COMMANDER, VENEZUELAN NAVY
VENEZUELAN NAVAL ACADEMY, 1965

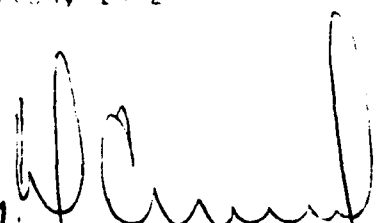
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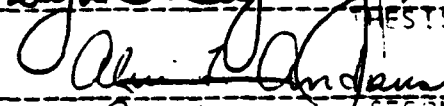
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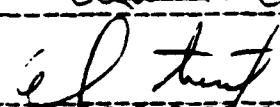
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I. INTRODUCTION

A war game is a dynamic presentation of military actions executed in such a way that one or more human participants can exercise control and take decisions against the activities of opposing forces in a real or hypothetical scenario. There are essential elements in war games which distinguish them from other simulations of military activities. They are:

- a. Force command and control (the combat decisions) if the opposing forces are made by human decision-makers.
- b. These decision-makers must react to the evolution of the combat and exercise their capabilities and experience in order to take decisions that later will reflect their accuracy or not in the outcome of the battle.

These characteristics make war games perhaps the only medium available, short of war, efficient enough for evaluating and examining command decisions at every level as well as constituting a tool to identify and isolate problems such as weapons limitations, forces weakness, logistic requirements, command and control, etc., as they arise during the execution and conduct of the operations; and in addition, the affect of the environment where forces are supposed to enact. More generally, a war game is a simulation, which is operated in accordance with predetermined rules, data, and procedures for selected aspects of a conflict situation.

Simulation also provides a means for gaining experience, and the development of analytical expertise and awareness of the systems available, without paying the penalties of a real world conflict.

In order to fulfill their objectives, war games must be realistic and reflect at every moment the sense of real conflict situations, where the players have the opportunity to exercise their skills in dealing with the variables in play. The author believes that one of the key points which contributes to the realism of the games is to have an accurate Damage Assessment procedure, from which people involved in the game could evaluate operational and tactical outcomes with respect to the decisions that they make.

In order to obtain this degree of realism, the people in charge of the damage assessment role must have valid and accurate information pertaining to vulnerability, reliability, accuracy and destructive power of weapons systems under consideration, as well as an unbiased appreciation of the power and weakness of the opposing forces. In addition, the players must be able to use the outcomes of the damage assessment process to develop capabilities and techniques to evaluate the performance effectiveness of the systems on hand and to take the optimal decision that the tactical situation and the ongoing operations require.

For the case of naval forces in a combat situation, it is necessary to have a means of assessing the damage to the

combatants as a function of their respective forces composition. The specification of such a damage function is not an easy task because of the varied roles that different force types play; and also because the interactions between force types can vary considerably with respect to the different characteristics which will add more complexity to the model.

This work presents a particular view of Surface Damage Assessment by considering Missile and Gunfire. The author uses a Monte Carlo technique in a stochastic process in which two opposing surface forces of one or more ships (Blue and Red) engage in a gun and missile battle.

The expected damage for each force is assessed by considering the following variables:

- A. Expected Damage Given One or More Hits.
- B. Target Aspect (angle).
- C. Rate of Weapons Fire.
- D. Jamming Factor.
- E. Weapon Hit Probability as a Function of Range.
- F. Sea State.

The simulation program combines a deterministic expected value model and chance elements by means of a routine written in Fortran IV using an IBM 3060 computer.

The Damage Assessment model will now be discussed in detail, followed by a description of how the variables were considered. A practical example of its implementation is then shown.

II. DAMAGE MODEL

This chapter presents in detail the method followed in the development of the model. It also describes the factors taken into consideration in order to keep a sense of both realism and consistency.

The absence of a mathematical expression which permits the damage calculations and the variety of variables and parameters which has to be considered (e.g., platforms type, weapons, number of units) make the work difficult to accomplish, and it requires a great deal of research and real world experience to give the analyst the necessary background to cover all the areas of importance.

A. GUNFIRE DAMAGE MODEL

The work was conducted using the bibliography available at the library of the Naval Postgraduate School. However, most of the material in this field is classified. Therefore it was necessary to create hypothetical, but reasonable, data in order to build the foundations to support the model. The damage calculations are realistic, but will not be necessarily accurate in detail until experimental data are obtained. The factors which were considered in the model are:

1. Target Aspect Factor (angle)
2. Hit Probability as a Function of Range

3. Expected Damage Given a Hit as a Function of Target Size
4. Sea State
5. Deceptive Jamming Factor
6. Weapons Rate of Fire

Each factor is presented in the following section with discussion as to how they were considered for model purposes.

1. Target Aspect Factor

For the purpose of the model, target aspect is the relative position of the target with respect to the opposing ship. It is defined as:

The smallest angle between the line of fire and the center line of the target ship.

The line of fire is the bearing of the point of aim from the center of the firing ship. If this line is within a given number of degrees, it will be an indication of the relative position of the target and the firing ship will have an angular value which reflects the characteristics of the ships considered.

In order to implement this factor into the model, a target size was chosen that was the average for the most common ships.

length 500 feet

width 55 feet

The next step was to combine target angle with the range in order to obtain a numerical value called Target Aspect

Factor which reflects how the relative angle and range of the target, with respect to the attacking ship, will affect the accuracy of the delivery of weapons.

The next step was to have a base range which was used as indication of position of the forces. It was necessary to split the range in three sections as follows:

Long Range = $.9 \times$ Effective weapon range

Medium Range = $.6 \times$ Effective weapon range

Short Range = $.3 \times$ Effective weapon range

When the target range falls closest to the above values, then it is said that the target is at long, medium, or short range, respectively.

In order to combine Target Range and Target Angle, a mathematical relationship was developed by considering: Target Length, Target Width, and Target Angle, and the value of the angle formed by the projectile trajectory and target vertical plane. This angle will be called from now on the "Incidence Angle" (Ω). In order to determine the values for the incidence angle, it was found in the trajectory tables for 6 inch guns that this value changes with the range. The values were selected for long, medium, and short range; see Figure 1.

For long range, the Ω value was 45 degrees. For medium range the Ω value was 15 degrees. For short range the Ω value was 3 degrees. The relationships expressed above are:

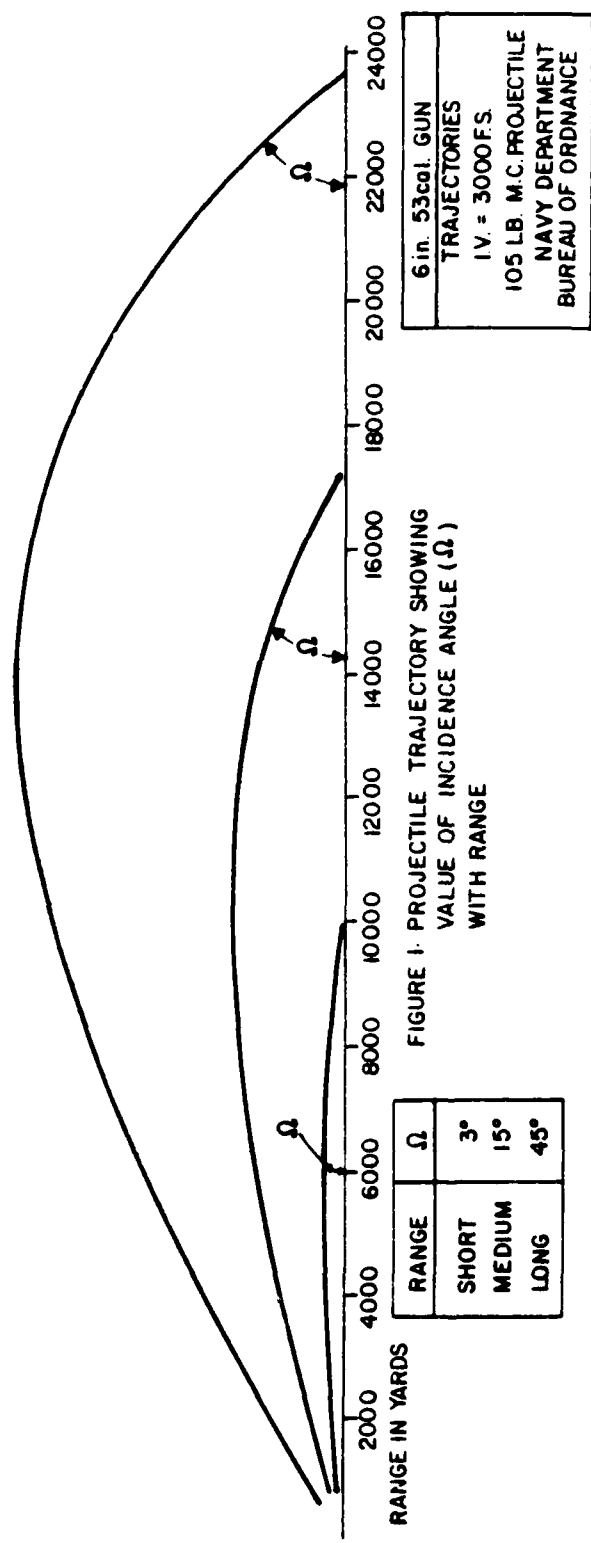


FIGURE 1. PROJECTILE TRAJECTORY SHOWING
VALUE OF INCIDENCE ANGLE (Ω)
WITH RANGE

| RANGE | Ω |
|--------|----------|
| SHORT | 3° |
| MEDIUM | 15° |
| LONG | 45° |

a. Short Range

$$\frac{1}{2} \sin (\text{Theta}) + w \cos (\text{Theta})$$

b. Medium Range

$$1 \sin (\text{Theta}) + \cos (\text{Theta}) [w = 1 \sin (\text{Omega})]$$

c. Long Range

$$1 \sin (\text{Theta}) + \cos (\text{Theta}) [w + 1 \sin (\text{Omega})]$$

Where:

Omega = Incidence Angle

Theta = Target Angle

l = Target Length

w = Target Width

The values taken for Theta are 0, 15, 30, 45, 60, 75, 90 degrees.

Once the computations were completed and the values normalized, a matrix of target aspect factors was constructed as it is shown below in Table 1.

TABLE 1: Target Aspect Factors

| | <u>0</u> | <u>15</u> | <u>30</u> | <u>45</u> | <u>60</u> | <u>75</u> | <u>90</u> |
|---------------|------------|-------------|-------------|-------------|-------------|-------------|-----------|
| <u>Short</u> | <u>.22</u> | <u>.47</u> | <u>.69</u> | <u>.86</u> | <u>.90</u> | <u>1.02</u> | <u>1</u> |
| <u>Medium</u> | <u>.37</u> | <u>.61</u> | <u>.82</u> | <u>.96</u> | <u>1.05</u> | <u>1.06</u> | <u>1</u> |
| <u>Long</u> | <u>.80</u> | <u>1.04</u> | <u>1.20</u> | <u>1.28</u> | <u>1.27</u> | <u>1.17</u> | <u>1</u> |

The above matrix shows the target factors values per range and per target angle. The reason for their behavior is because gunnery errors in range and deflection can usually be described by a normal distribution which is also represented by two parameters, Mean Error (ME) and Probably Error (PW). In the absence of bias, Mean Error is equal to Probable Error (ME=PE). In this case, then, the distribution of the errors is circular and the ME and PE are called Circular Error Probable (CEP). But in our case bias is present due to the delivery error of guns in the system and the distribution is Elliptical Normal with the deflection error smaller than range error. The result is that at long range when omega is greatest the target aspect factor is much less than at short range when the gunfire is nearly horizontal. That is the reason why the Target Aspect Factor decreases in relativity as the range increases.

2. Hit Probability as a Function of Range

Once again due to non-availability of real data, it was necessary to find a rational way to obtain numerical values which represent how accurate the weapons systems are and how they are affected by the range. Assuming that the probability of impact of the weapons decreases as the range increases, a graphical relationship was developed in order to have a source that would vary the values of hit probability with respect to range. For doing this two gun types were chosen (5 inch and 4.5 inch); see Figures 2 and 3.

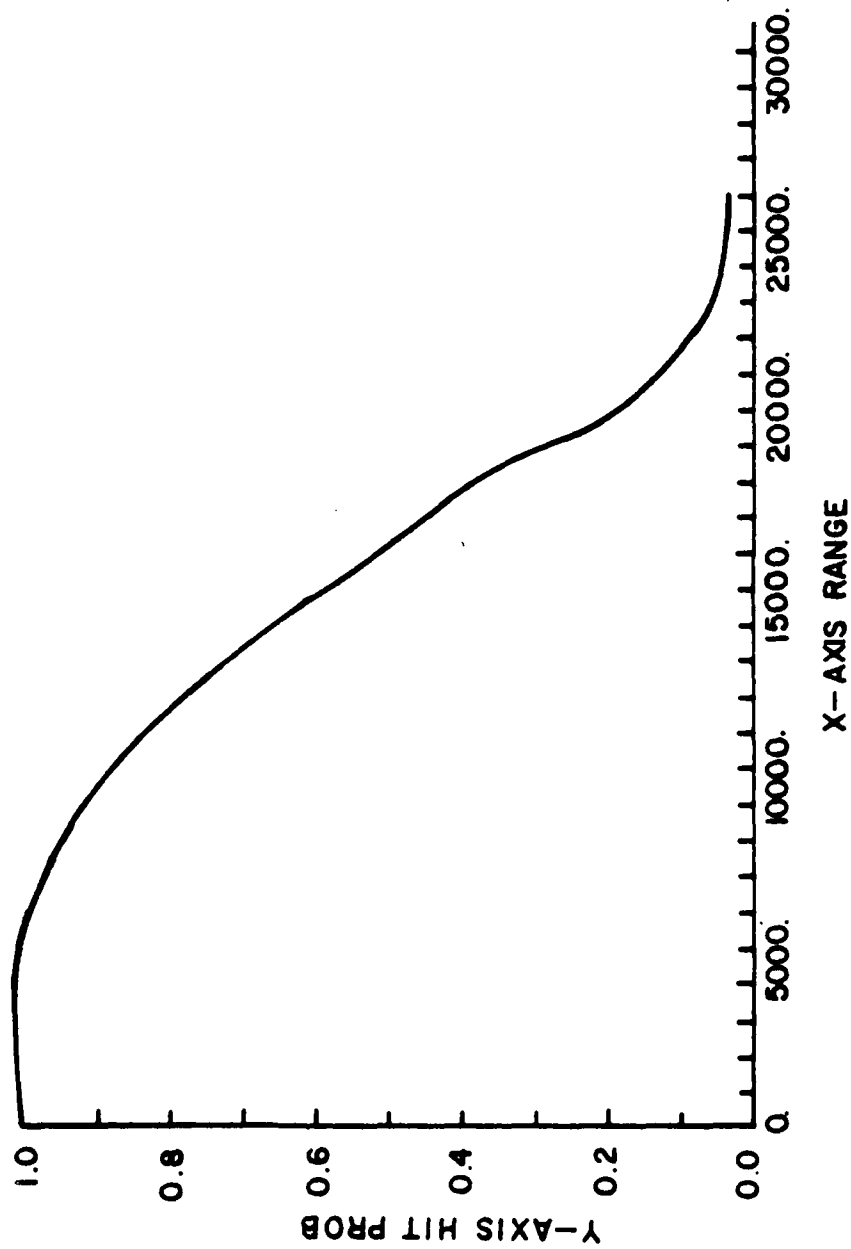


Figure 2. Graphical Representation of Hit Probabilities as a Function of Range for Gunfire (Blue)

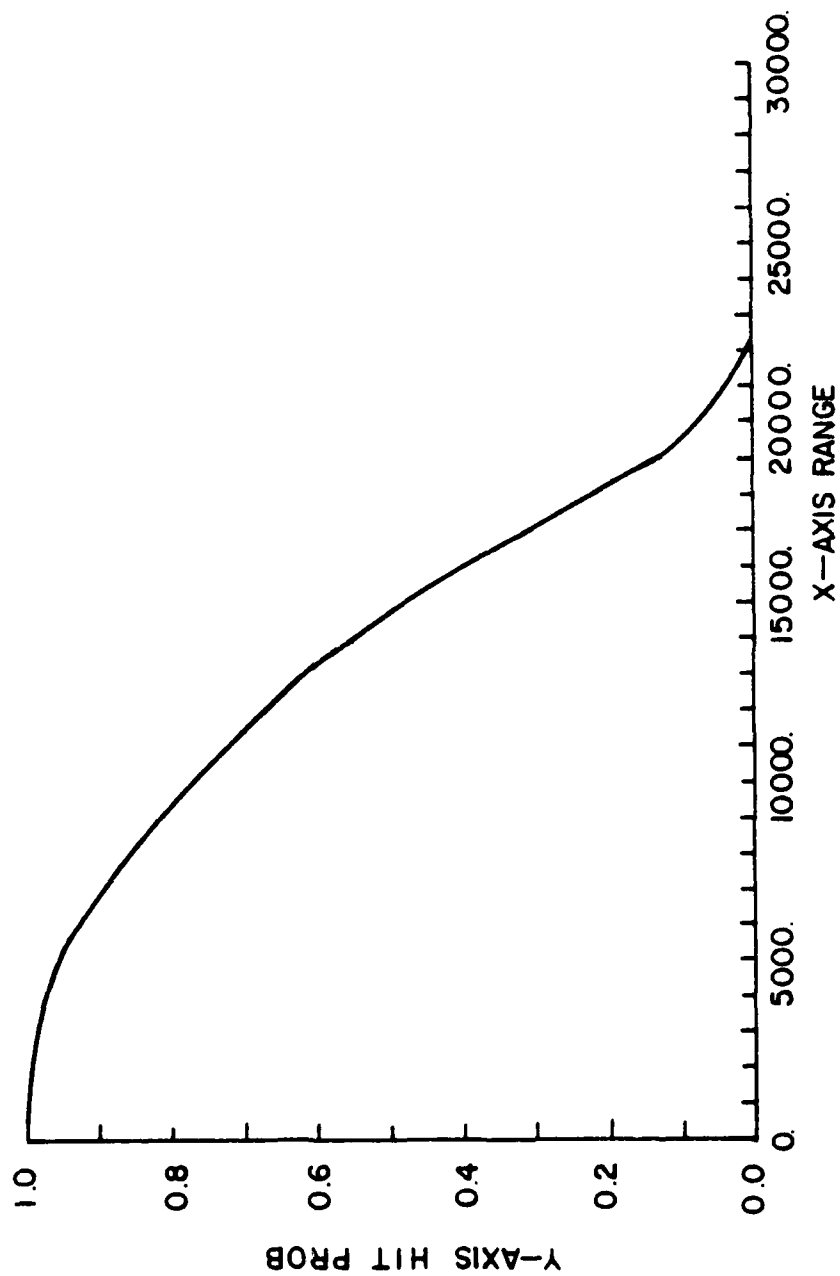


Figure 3. Graphical Representation of Hit Probabilities as a Function of Range for Gunfire (Red)

3. Expected Damage Given A Hit

For this a relationship was developed such that as the size of the target increases the expected damage due to critical hits will decrease. In other words, the degree of target vulnerability is inversely proportional to the target size. See Figure 4 and Figure 5 for Blue and Red, respectively.

4. Sea State

The sea condition is a well known factor which degrades the effectiveness and accuracy of the gunfire, where the personal capabilities and the stabilizations systems are down graded enough to considerably reduce the overall effectiveness of the system. The scale was used as a reference point to build a factor table which would have an equivalent factor for each Beaufort state. For values equivalent to Beaufort Scale 5 or above, the effectiveness of surface forces engagement are highly diminished. See Table 2.

5. Deceptive Jamming Factor

Deceptive jammers interfere with enemy gunfire control, the guidance of the missile weapons, and their acquisition systems. The effect of deceptive jammers is to increase the probable error and also to deflect the aimpoint back behind the center of the target with the results that the hit probability decreases. For the purpose of the model when deceptive jamming is being employed, a random

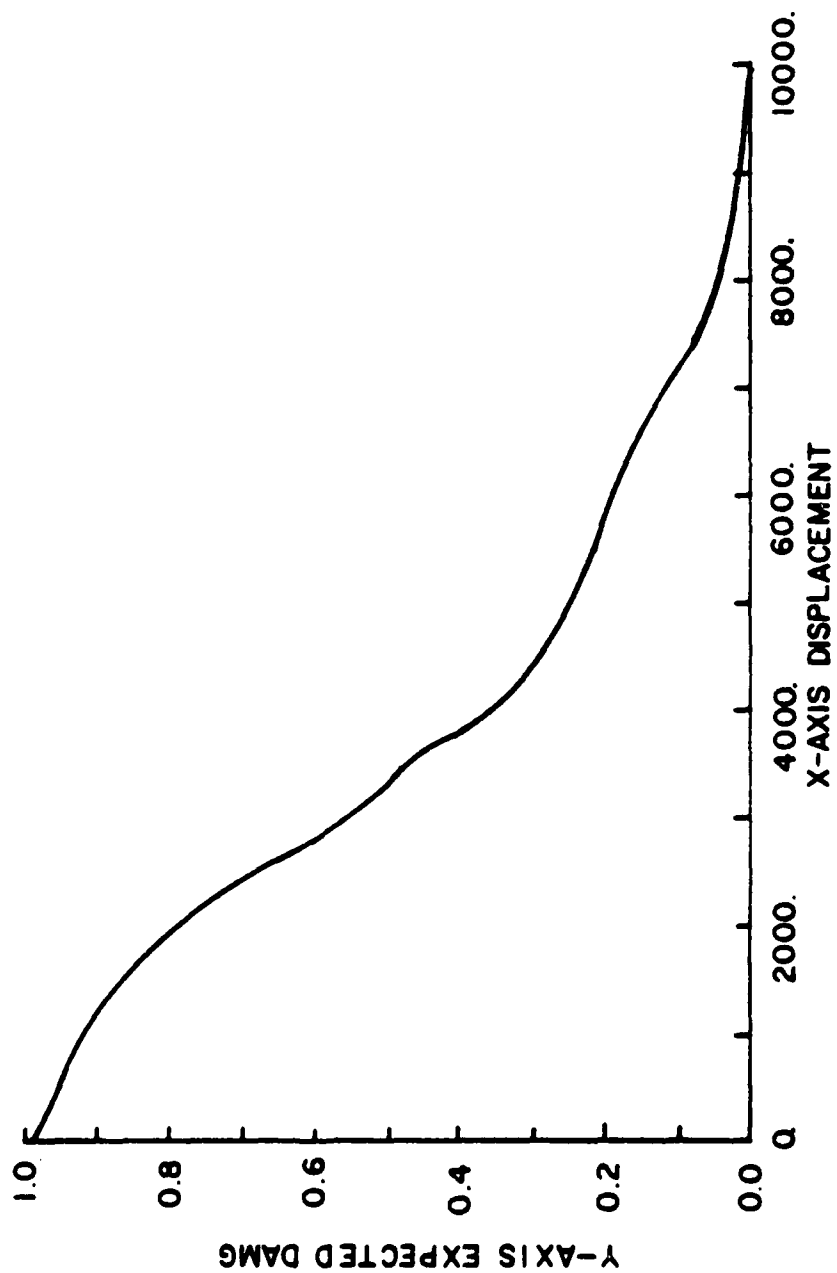


Figure 4. Expected Damage vs Range for Gunfire (Blue)

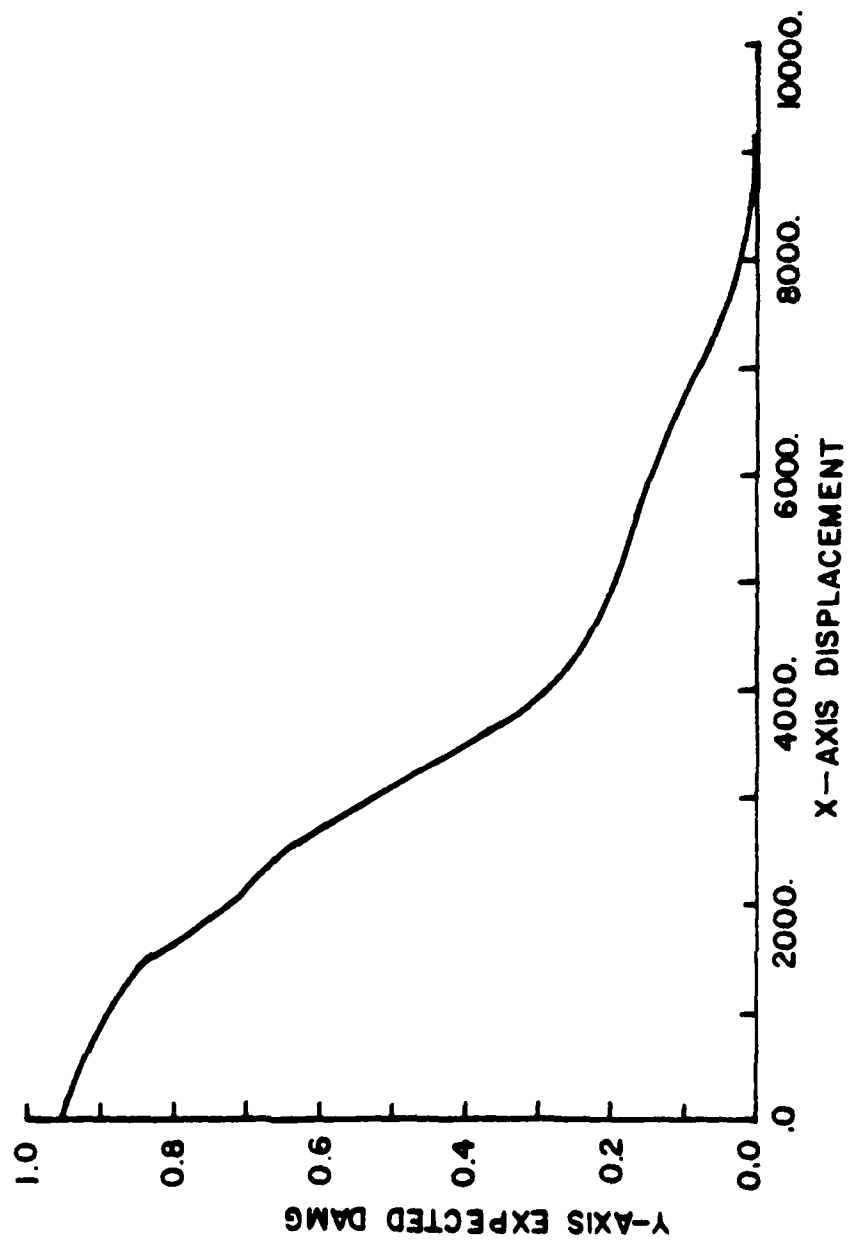


Figure 5. Expected Damage vs Range for Gunfire (Red)

TABLE 2. Beaufort Scale and Equivalent Sea State Factor

| <u>Beaufort</u> | <u>Sea State Factor</u> |
|-----------------|-------------------------|
| <u>0&1</u> | <u>1.0</u> |
| <u>2</u> | <u>.8</u> |
| <u>3</u> | <u>.7</u> |
| <u>4</u> | <u>.7</u> |
| <u>5</u> | <u>.6</u> |
| <u>6</u> | <u>.5</u> |
| <u>7</u> | <u>.4</u> |
| <u>8</u> | <u>.4</u> |
| <u>9</u> | <u>.3</u> |
| <u>10</u> | <u>.3</u> |
| <u>11</u> | <u>.2</u> |
| <u>12</u> | <u>.1</u> |

Aircraft Carriers and Battleships.

Total Life (slife) = Displacement/100

Carriers.

Total Life (slife) = Displacement/70

Destroyers and Frigates

Total Life (slife) = Displacement/30

Corvetes and below.

number is chosen between .5 and 1.0. This value represents in the model a reduction in the weapons effectiveness which goes from a maximum effect of .5 to a minimum effect of 0. There is no consideration of multiple deceptive jammers in the model.

6. Rate of Fire

One of the questions which varies with operational circumstances is, what rate of fire should be used? This factor depends upon the tactical situation, state of training, enemy characteristics, magazine capacity, etc.; but the rate of fire must be consistent with the individual ships' circumstances, and will often not be as much as the theoretical, or gunnery range maximum.

In war games it is common that the players expect unrealistically high rates of fire, since the more rounds that are fired accurately during the action, the higher the cumulative kill probability is. When different firing rates are considered, fewer rounds expended at a high rate of accuracy may be more effective than more rounds expended at a lower rate of accuracy.

For this model in particular, the rate of fire that will be allowed is an input which has to be decided by the umpire, depending upon the tactical situation, state of training, and weapons reliability.

B. GUN FIRE DAMAGE CALCULATIONS

It was necessary to create a numerical value which represents the idea of life of the target. This value also represents in the model the target's capabilities to sustain damage; it will be reduced each time a hit occurs. For this purpose the displacement of the target in tons was considered to represent, in a way more or less tangible, the life of the ship along with a factor to use as a divisor in order to get what is believed to give a realistic relationship between hits and damage. This divisor changes for different targets or platforms. The total life value is derived in the following way:

$$\text{Total Life (slife)} = \text{Displacement}/20$$

The damage computations are conducted with the following steps:

1. For each interaction, a value of expected damage is obtained. It is called Expected Damage per Move. The value is computed by means of the following expression.

$$\text{EDMM} = [\text{Edam}|\text{Hit}] * \text{Ph} * \text{Rf} * \text{Seast} * \text{Xjamm} * \text{Tagta}$$

Where:

EDMM = Expected Damage per Move.

EDAM|hit = Expected Damage Given a Hit Occurs.

PH = Hit Probability of the Weapon

RT = Rate of Fire During the Engagement.

Seast = Sea State

Xjamm = Deceptive Jamming.

Tagta = Target Aspect Factor.

2. The residual target life is computed applying the following linear expression.

$$RLIFE = RLIFE \left(1 - \sum_{L=1}^m EDMM \right)$$

3. The cumulative damage per move is simply the difference t life minus rlife.

$$CDPOINT = TLIFE - RLIFE$$

4. The percent floating capabilities is computed as follows.

$$FLOATC = (1 - CDPOINT/TLIFE) * 100$$

5. A coverage factor is required in order to establish how large the damage is to each ship's component along the target length.

$$SBAND = EDMM * TLENGTH$$

6. A location of where the target was hit was required and in order to do this the target length was considered as a base, ranging from zero (0) to five hundred (500), then a uniform random number was drawn. The number gives the physical location of the weapon hit on the target.

Once the hit place is determined, the next step is to find out which of the systems on board were knocked out or damaged. The hit place is considered the center. The upper bound of the hit will be the hit place plus half of the coverage factor, and the lower bound will be the hit place minus half of the coverage factor.

$$\text{DAMAGE AREA} = (\text{sband}/2 \leq \text{hplace} \leq \text{sband}/2)$$

An example of how hit placement, coverage factor, and target elements are determined is shown in Figure 6. Figure 6 is a sketch of a target type showing the target elements subject to suffering an amount of damage per move or during the engagement.

Line "A" shows where the target elements are placed along the target length from stern to bow.

Line "B" shows where the hit has occurred and how many target elements were subject to damage.

Let's suppose that the outcome of a uniform random number is 250. This number indicates that the place where the hit occurred was at 250' from stern to bow. The area of the ship suffering damage is given by the size of the Coverage Factor (SBAND) whose center is placed at hit place (HP). This physical dimension equals to $\text{SBAND}/2$ (250 ± 50).

The actual target elements which suffer damage are those which are located within the area between 200' and 300'. For this particular example they are:

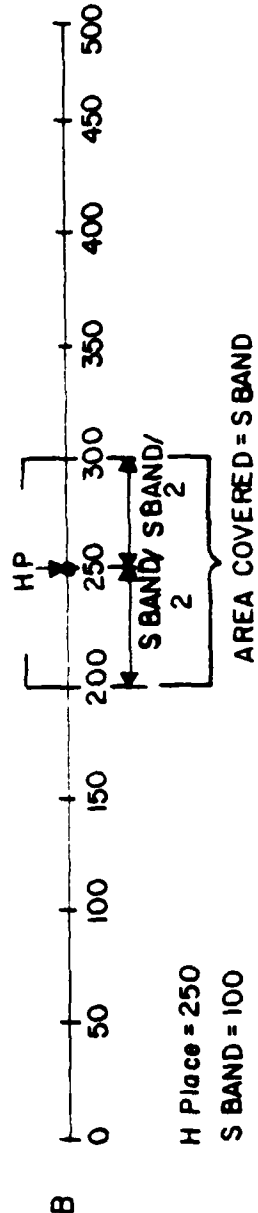
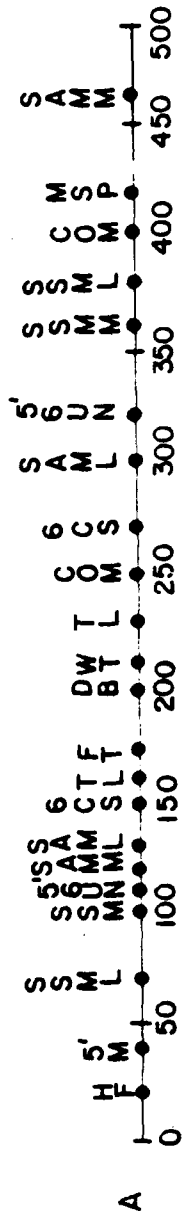
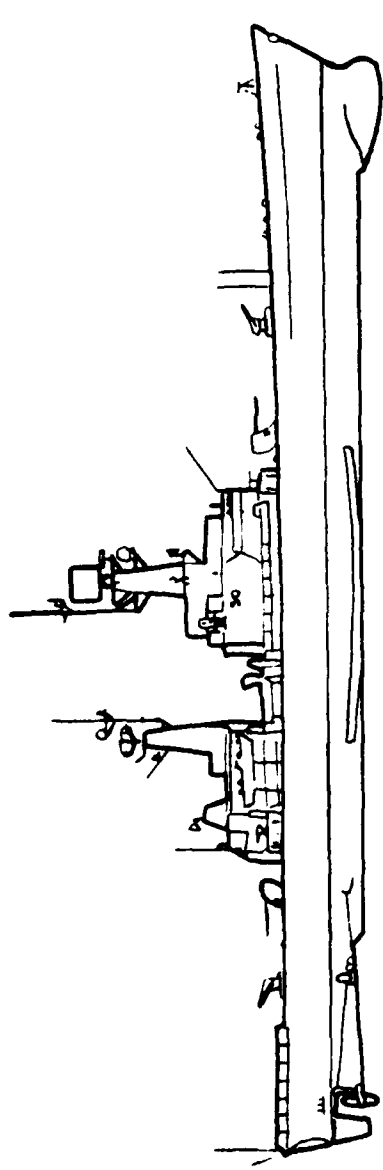


Figure 6. Graphical Representation of Target Placement (A) and Covered Area (B)

DAMAGE BRIGADE I
WATER TANK
TORPEDO LAUNCHER II
COMMUNICATION SYSTEMS (UHF-HF)
5" GUN CONTROL SYSTEM II
SURFACE-AIR MISSILE LAUNCHER II

A first step before the start of the game is to locate the target elements as they are actually positioned along the target length. Each element is given an initial condition, a location on the target, an identification number, and, the degradation factor. The degradation factor indicates the percent of damage each target element suffers if it is hit; the amount of damage is cumulative per move. There are twenty-two target elements in the sample table shown below, Table 3.

Table 3 was used for a Red Target; one similar for Blue, but with different distribution elements and different factors was also designed.

After each move the players and the game director will have available a computer output showing the residual capability values of all the target's elements. These will be the input for the next move. Also a summary, called History, will be available with all the computations done during the game.

TABLE 3. Target Elements Distribution

| <u>Target Element</u> | <u>Target Ident.</u> | <u>Target Place</u> | <u>Target Condition</u> | <u>Target Damage Factor</u> |
|---------------------------|--------------------------|-------------------------|-----------------------------|-------------------------------------|
| HELO FUEL | 1 | 10 | 28000 gals. | .25 |
| 5' MAGAZINE | 2 | 40 | 100% | .50 |
| SSML I | 3 | 70 | 100% | .50 |
| SSM MAGAZINE | 4 | 100 | 4 | .50 |
| 5' GUNd | 5 | 110 | 100% | .50 |
| SAM MAGAZINE | 6 | 120 | 9 | .50 |
| SAML I | 7 | 130 | 100% | .50 |
| GUN C SYSTEM | 8 | 150 | 100% | .50 |
| TORPEDO L I | 9 | 160 | 100% | .50 |
| FUEL TANK | 10 | 170 | 360 tons | .25 |
| DAMGE BRIG. I | 11 | 200 | 100% | .50 |
| WATER TANK | 12 | 210 | 20000 gals. | .25 |
| TORPEDO L II | 13 | 230 | 100% | .50 |
| COM. HF UHF | 14 | 250 | 100% | .50 |
| GUN C SYSTEM II | 15 | 270 | 100% | .50 |
| SAML II | 16 | 300 | 100% | .50 |
| 5' GUN | 17 | 320 | 100% | .50 |
| SSM MAGAZINE | 18 | 360 | 4 | .50 |
| SSM L II | 19 | 380 | 100% | .50 |
| COM LF VHF | 20 | 400 | 100% | .50 |
| MAX SPEED | 21 | 420 | 38K | .25 |
| SAM MAGAZINE | 22 | 460 | 9 | .50 |

The damage to certain ship elements like Surface Radar, Electronic Countermeasures (passive and active), Air Radar, and the Helo, considered separately as a kill-no-kill calculation.

C. MISSILE DAMAGE MODEL

The missile damage model basically follows the same structure as the gun fire model with slight differences in the factors under consideration. The factors considered are:

- a. Expected Damage per Missile Hit as a Function of Target Size.
- b. Missile Hit Probability as a Function of Range.
- c. Target Aspect.
- d. Sea State.
- e. Number of Missile Impacts.
- f. Warhead Factor.

These will be considered in more detail as follows.

1. Expected Damage Given a Missile Hit (range)

As in the Gun Fire case, a set of values assuming a relationship between the range and the damage due to critical hits was developed from hypothetical data.

In Figure 7 this relationship is presented graphically showing how the damage due to critical hits decreases as the target size increases. One of these graphs was created for both Blue and Red forces.

2. Missile Hit Probability as Function of Range

This is similar to the way it was treated for the Gun Fire case. It's graphical consideration is shown in Figure 8.

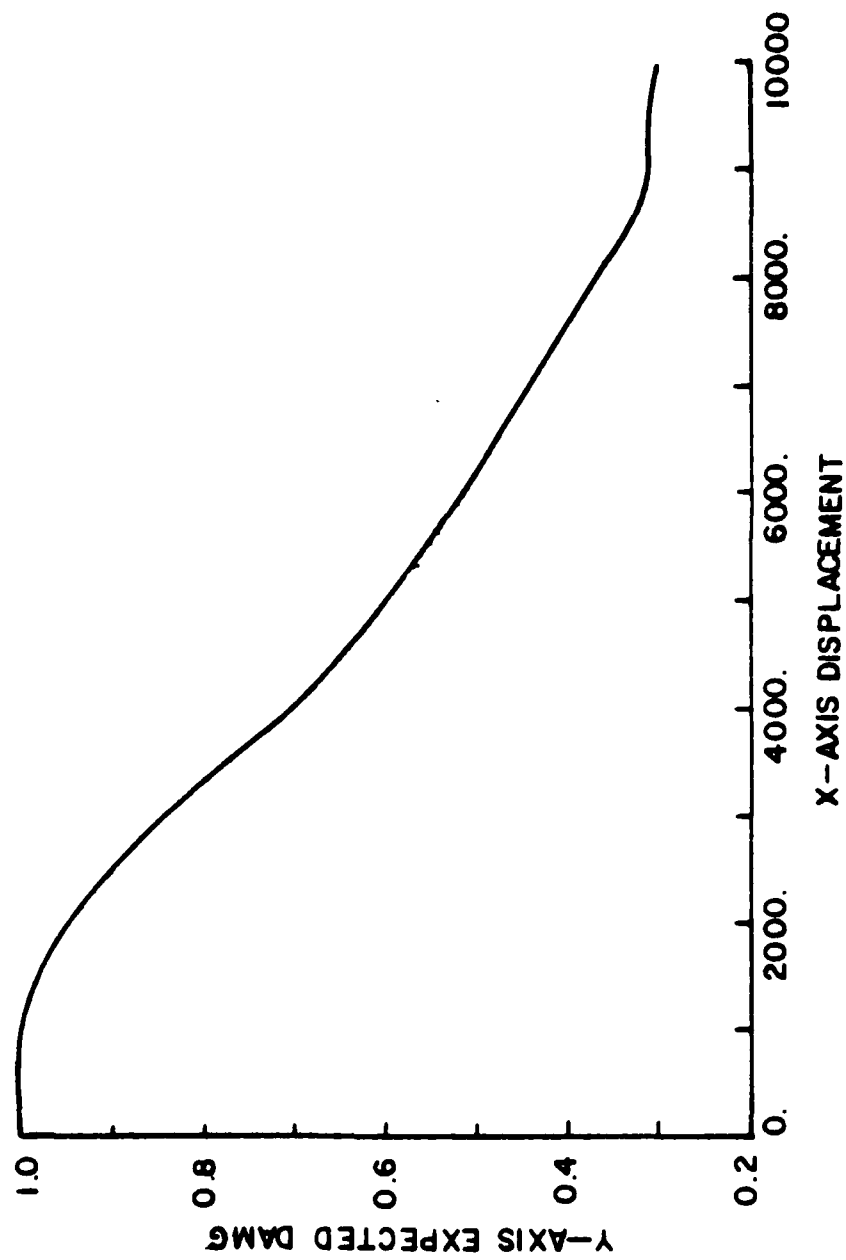


Figure 7. Expected Damage vs Range for Missile Fire (Blue & Red)

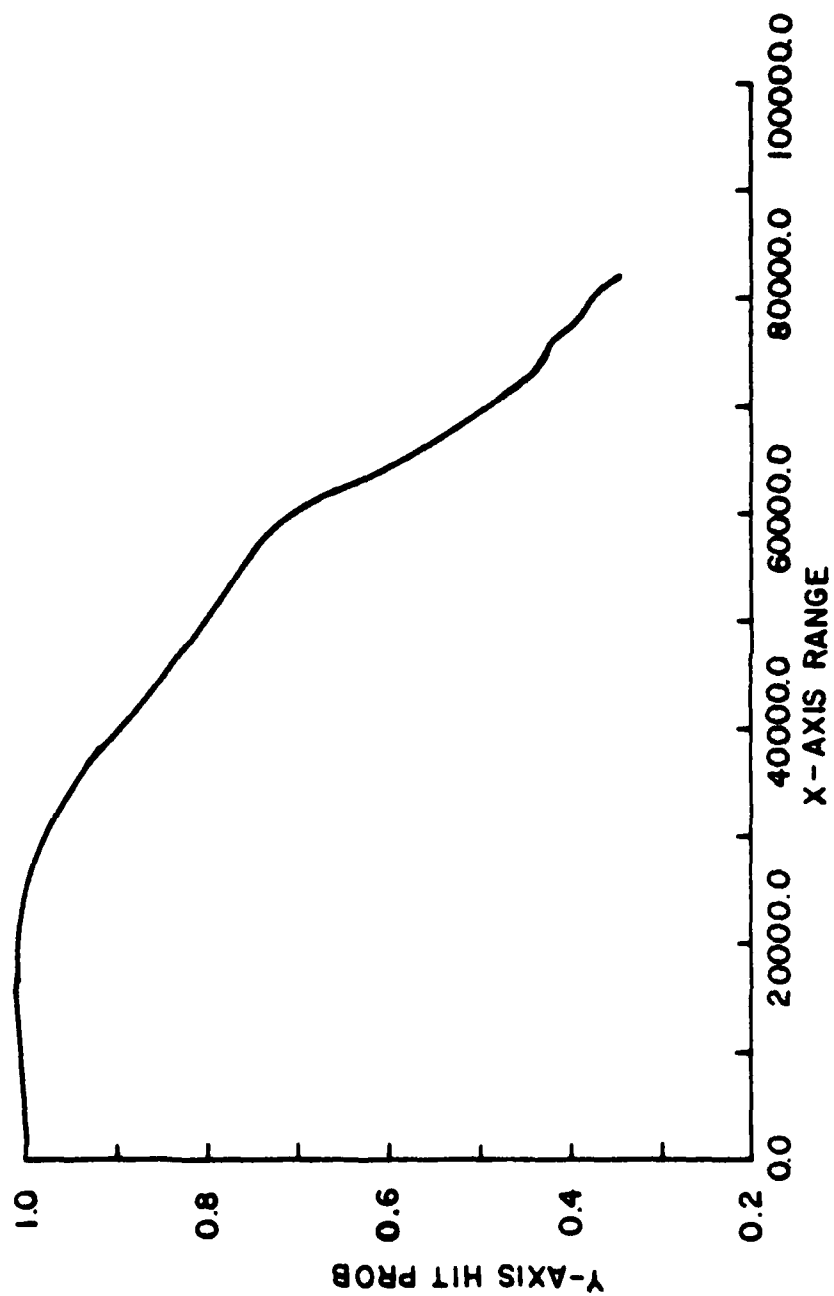


Figure 8. Graphical Representation of Hit Probabilities as a Function of Range for V-missile Fire (Blue & Red)

3. Target Aspect Factor

The missile model included the target aspect factor with a constant value equal to one (1). This is presented in this simple form because it will require further analysis which should be considered later as an improvement for the model.

4. Deceptive Jamming

This factor is considered in the same way it was for the Gun Fire case.

5. Missile Impacts

This factor was included as a multiplicative factor depending on the number of missiles remaining alive after considering the defense capabilities of the target ship. It was thought that a single target is able to shoot down the first incoming missile with probability equal to 0.7 and shoot down a second incoming missile with probability of 0.25. Using the technique of drawing a random number and comparing it with the above probabilities, we assess how many of the detected missiles constitute a surviving threat to the target ship.

Once we know the remaining missiles alive, we again pull a random number. By comparing it with the missile kill probability (0.7), we establish how many of them make impact on the target.

6. Warhead Weight Factor

Knowing that the destructive power of a missile mainly depends on the explosive charge it carries, the inclusion of this aspect was considered of great importance.

This factor was obtained as a ratio between the actual missile warhead weight and a warhead weight type. In this case, the weight of 250 pounds was taken as standard. This value is fed into the general expression to calculate the cumulative damage.

$$WHEAD = \text{MISSILE WARHEAD WEIGHT} / 250$$

Where:

WHEAD = Warhead Factor

D. MISSILE DAMAGE CALCULATIONS

For missile damage calculations the following expression was used in order to compute the Expected Damage per Move:

$$EDMM = (EMHIT) * PHIT * IMPAT * XJAMM * WHEAD * SEAST * TAGTA$$

Where:

EDMM = Expected Damage per Move

EMHIT = Expected Damage per Missile Hit

PHIT = Missile Hit Probability

IMPAT = Missile Impacts on Target

XJAMM = Deceptive Jamming Factor

WHEAD = Warhead Weight Factor

TAGTA = Target Aspect Factor

SEAST = Sea State

After the expected damage per move has been computed, the rest of damage calculations are the same as in the gunfire model.

III. PROGRAM DESCRIPTION

A computer program was written to support the model. The present chapter will explain in detail how it was used and how the data was handled. The listing of the computer program is presented in Appendix A.

The program is suitable to assess damage for any number of targets (in the example $N = 4$), one at a time in two versions, Gun Fire and Missile Fire.

A. INPUT

Two sets of data were used for each force, independently, and were called Blue Datal, Blue Data2, Red Datal, and Red Data2. Those sets of data are shown in the appendix. They contain the following information in the order they appear.

1. Datal

| | |
|---------------------|--------|
| NAME OF THE SHIP | NS |
| TARGET RANGE | KRANGE |
| TARGET LENGTH | TARLE |
| TARGET WIDTH | TARWI |
| TARGET DISPLACEMENT | TONS |
| TARGET ANGLE | THETA |
| DEFENSE FACTOR | DIFAC |
| SEA STATE | SEAST |
| RATE OF FIRE | SRT |

| | |
|---------------------------------|--------|
| MISSILE HIT PROB. | ZPHIT |
| MISSILE WARHEAD WEIGHT | HWEIT |
| GUNFIRE RANGE | R1 |
| MISSILE FIRE RANGE | R2 |
| MAXIMUM GUN FIRE RANGE | MRANGE |
| DISPLACEMENT | DISP |
| EXPECTED DAMAGE/HIT | EDMH |
| TARGET RANGE | TAR |
| GUN HIT PROBS. | YHIT |
| SHORT RANGE TAGTA FACTOR | sFAC |
| MEDIUM RANGE TAGTA FACTOR | mFAC |
| LONG RANGE TAGTA FACTOR | ZFAC |
| TARGET ELEMENT IDENTIFICATION | IDENT |
| TARGET ELEMENT PLACE | TPLACE |
| TARGET ELEMENT DEGRATING FACTOR | TEFAC |

2. Data2

| | |
|--------------------------|--------------------|
| TARGET ELEMENT CONDITION | TCOND |
| TOTAL LIFE | SLIFE |
| REMAINING LIFE | RLIFE |
| CCUMULATIVE DAMAGE | SUM |
| HIT PLACE | HPLACE |
| GAME TIME | GTIME |
| SEEDS | IX,IX1,IX2,IX3,IX4 |

B. PROGRAM RUN

The program is fed with Data1 and Data2 per side each time we want to establish the amount of damage sustained for a target after a move has occurred. This procedure is to be done for each target separately. For the subsequent moves it is necessary to introduce the changes required by the new tactical conditions and with the prior damage results.

C. PROGRAM OUTPUT

The outcome of each engagement will consist of two printed outputs which will be stored in files called History1 and History2 for each side, and will be a compilation of the moves. In order to identify to which side the file corresponds, a letter B (blue) or R (red) will be placed before the word history.

1. HISTORY1 File

This file will contain the following information:

Type of Engagement (Gun or Missile Fire)

Target Name

Number of Missiles Detected

Number of Missiles Shotdown

Number of Missiles Alive

Number of Missile Impacts on Target

Target Aspect Factor

Expected Damage per Move

Remaining Life

Cumulative Damage

Floating Capabilities

Total Life

Hit Probability (Gun or Missile) of Engagement

Hit Place

Deceptive Jamming Factor

Coverage Factor

Target Elements Hit in the Move

Residual Conditions of all Target Elements

2. HISTORY2 File

This file will contain the information concerned with the residual conditions of the targets considered in the game. This information will become the initial conditions for subsequent moves.

IV. RESULTS AND FUTURE IMPROVEMENTS

A. RESULTS

The objective of the model, namely to obtain more rapid, accurate and realistic results during the damage assessment process, has been achieved. By giving the results to the game director and to each player, more time will be gained for tactical decisions and play. As reliable, validated inputs are provided, the model will present realistic combat outcomes to assist in the development of improved tactical doctrine.

B. FUTURE IMPROVEMENTS

The present model was developed as a tool for war gaming damage assessment that provided accuracy, realism, and rapid computations during the conduct of the game.

Future improvements should include the following:

1. Validation

The model was developed and tested to a great extent with hypothetical data due to the absence of real or experimental data. Such data should be acquired to confirm or improve the model's accuracy and reliability.

2. Tactical Improvements

- a. The model now only considers a surface naval engagement involving Gun and Missile fire. The expansion of the model to include other important aspects, such as the ASW Warfare, AAW Warfare, Torpedo Attack, and Mines will enhance the utility of the model.
- b. The expansion of the model by including the possibility of treating more than one platform at the same time will accelerate the Damage Assessment process.
- c. The consideration of the target aspect factor in a missile engagement is an important future refinement for accuracy, and in addition will show how this factor affects the outcome of the engagement.
- d. The inclusion of the effects of damage to the Command Control and Communications will introduce in the game a factor of vital importance which is often overlooked during the conduct of fleet exercises and war games.

APPENDIX A

This appendix contains a list of variables in the order they appear in the program, a listing of the program, and inputs for force blue and red.

LIST OF VARIABLES

| | |
|--------|--|
| SLIFE | TARGET TOTAL LIFE |
| TONS | TARGET DISPLACEMENT |
| XJAMM | DECEPTIVE JAMMING FACTOR |
| KRANGE | DETECTION RANGE |
| THETA | TARGET ASPECT ANGLE |
| MRANGE | MAXIMUM RANGE |
| TAGTA | TARGET ASPECT |
| SFAC | SHORT RANGE TARGET ASPECT FACTOR |
| TFAC | MEDIUM RANGE TARGET ASPECT FACTOR |
| ZFAC | LONG RANGE TARGET ASPECT FACTOR |
| DISPR | DISPLACEMENTS TYPE |
| FEDHR | EXPECTED DAMAGE AS FUNCTION OF TARGET SIZE (GUN) |
| JRGED | TARGET RANGE |
| SRF | RATE OF GUN FIRE |
| SEAST | SEA STATE |
| PHIT | GUN HIT PROBABILITY |
| NS | TARGET NAME |
| NM | NUMBER OF MISSILES DETECTED |

| | |
|--------|---|
| PK1M | PROBABILITY OF KILL FIRST INCOMING MISSILE |
| PK2M | PROBABILITY OF KILL SECOND INCOMING MISSILE |
| DIFAC | TARGET ANTI-MISSILE DEFENSE FACTOR |
| SDC | TARGET ANTI-MISSILE DEFENSE CAPABILITY |
| MALIVE | NUMBER OF MISSILES ALIVE |
| IMPAT | NUMBER OF MISSILE IMPATS ON TARGET |
| WHEAD | MISSILE WARHEAD WEIGHT FACTOR |
| HWEIT | MISSILE WARHEAD WEIGHT |
| EMHIT | EXPECTED DAMAGE PER MISSILE HIT |
| SBAND | COVERED AREA |
| PHB | HIT PROBABILITY AS FUNCTION OF RANGE (GUN) |
| TARLE | TARGET LENGTH |
| CDMPO | CCUMULATIVE DAMAGE PER MOVE |
| RLIVE | TARGET REMAINING LIFE |
| FLCAP | TARGET FLOATING CAPABILITIES |
| HPLACE | HIT PLACE |
| HALF | HALF COVERED AREA |
| UHALF | UPPER BOUND COVERED AREA |
| THALF | LOWER BOUND COVERED AREA |
| HLPK | HELO DAMAGE PROBABILITY |
| PCPK | ECM DAMAGE PROBABILITY |
| SRPK | SURFACE RADAR DAMAGE PROBABILITY |
| ARPK | AIR RADAR DAMAGE PROBABILITY |
| ACPK | ECCM DAMAGE PROBABILITY |

```

C*****
C** COMPUTER PROGRAM OF A DAMAGE ASSESSMENT MODEL OF A SURFACE EN
C** GAGEMENT BETWEEN TWO FORCES (RED & BLUE ) WITH MISSILE AND GUNFIRE
C**
C** * BY COMMANDER MARIO IVAN CARRATU MOLINA *
C** " ARNADA REPUBLICA DE VENEZUELA "
C** * NAVAL POSTGRADUATE SCHOOL *
C** MONTEREY, CALIFORNIA ***** MARZO 1982
C**
C** COMMON EDHR(25),DISPR(25),SPAC(10),TFAC(10),ZPAC(10),KRNGE,
C** THETA,KRNGE,TA,SEAST,PHB(25),JRGEB(25),PHR(25),JRGEB(25),
C** EDHB(25),DISPB(25),TCOND(4,22),IDENT(4,22),TPLACE(4,22),IX1,IX2,
C** TARLE,TA,WHIT(25),RLIFE,R1,R2,ZPHIT,DISP,EDMH,TAR,WHIT,R12,DIFAC,NH,WHHEAD,
C** RT1(20),GTIME,RT3,HWBIT,TEFAC(4,22),NS
C*****
C** MODEL INPUT DATA
C**
C** NAMELIST/ DATA1/ KRNGE, TONS, EDHR, DISPR, SPAC, TFAC, ZPAC, KRNGE, THETA,
C** SEAST, PHB, PHR, JRGEB, EDHB, DISPB, IDENT, TPLACE, TEFAC, TARLE,
C** TARH1, SRP, R1, R2, ZPHIT, DISP, EDMH, TAR, WHIT, R12, DIFAC, NH, WHHEAD,
C** HWBIT, NS
C** NAMELIST/ DATA2/ TCOND, SLIFE, RLIFE, SUM, HPLACE, GTIME, IX, IX1,
C** IX2, IX3, IX4
C** GTIME=0.
C** KRNGE=0.
C** KRNGE=0.
C** DISP(1)=0.
C** EDHR(1)=0.
C** TAR(1)=0.
C** WHIT(1)=0.
C** DISP(1)=0.
C** TONS=0.
C** THETA=0.
C** SUM=0.
C** READ(5, DATA1)
C** READ(4, DATA2)
C** REWIND 4
C*****
C** COMPUTATION OF DAMAGE CAPABILITY POINTS OF TARGET ( LIPE)
C**

```


PAK000480
PAK000490
PAK000500
PAK000510
PAK000520
PAK000530
PAK000540
PAK000550
PAK000560
PAK000570
PAK000580
PAK000590
PAK000600
PAK000610
PAK000620
P

SLIPE= TONS/30
GENERATION OF UNIFORM RANDOM DEVIATES IN ORDER TO HAVE RANDOMIZE
JANNING FACTOR. (UNIFORM FROM 0 TO 1.)

CALL LRND(IY,Y,N,1,0)
YJANN=5*Y+.5
IF (KRNGE .LE. R1) GO TO 20
GO TO 30
20 WRITE(6,11) GUNFIRE ENGAGEMENT'
11 FORMAT(3X,64)NS
WRITE(6,64)NS
64 FORMAT(3X,1) TARGET NAME=',I4)
K=6
DO 1 I=1,K
IF(THETA.GT.15(I-1))GO TO 134

GO TO 40
1 CONTINUE
40 CONTINUE
SCALING MAXIMUM RANGE BY CONSIDERING 30,60,90 PERCENT OF MAX RANGE
AS SHORT,MEDIUM AND LONG RANGE RESPECTIVELY.

SHORT=MRNGE*.3
MDIUM=MRNGE*.6
LONG= MRNGE*.9

SELECTION OF TARGET ASPECT FACTOR (ANGLE) AS AFUCTION OF RANGE

IF (KRNGE .LE. SHORT)GO TO 42
IF (KRNGE .LE. MDIUM .AND. KRNGE.GT. SHORT)GO TO 50
IF (KRNGE .LE. MRNGE .AND. KRNGE.GT. MDIUM)GO TO 60
GO TO 80

42 TAGTA=SPAC(I)
GO TO 70
50 TAGTA=TPAC(I)
GO TO 70
60 TAGTA=ZPAC(I)
GO TO 70
70 WRITE(6,12)TAGTA

COMPUTATION OF EXPECTED DAMAGE GIVEN A HIT PER WEAPON

PAK000640
PAK000650
PAK000660
PAK000670
PAK000680
PAK000690
PAK000700
PAK000710
PAK000720
PAK000730
PAK000740
PAK000750
PAK000760
PAK000770
PAK000780
PAK000790
PAK000800
PAK000810
PAK000820
PAK000830
PAK000840
PAK000850
PAK000860
PAK000870
PAK000880
PAK000890
PAK000900
PAK000910
PAK000920
PAK000930
PAK000940

PAK00950
PAK00960
PAK00970
PAK00980
PAK00990
PAK01000
PAK01010
PAK01020
PAK01030
PAK01040
PAK01050
PAK01060
PAK01070
PAK01080
PAK01090
PAK01100
PAK01110
PAK01120
PAK01130
PAK01140
PAK01150
PAK01160
PAK01170
PAK01180
PAK01190
PAK01200
PAK01210
PAK01220
PAK01230
PAK01240
PAK01250
PAK01260
PAK01270
PAK01280
PAK01290
PAK01300
PAK01310
PAK01320
PAK01330
PAK01340
PAK01350
PAK01360
PAK01370
PAK01380
PAK01390
PAK01400
PAK01410
PAK01420

```

C      DO 2 I=1,20
      IF (TOMS.LE.DISPR(I)) GO TO 3
      CONTINUE
      A=TOMS-DISPR(I-1)
      B=DISPR(I)-DISPR(I-1)
      C=A/B
      A=EDHR(I)-EDHR(I-1)
      B=C*A
      PEDHR=EDHR(I-1)+B

CCCCC
      DETERMINATION OF HIT PROBABILITIES AS A FUCTION OF RANGE (5 INCHES)

      M=15
      DO 8 I=1,M
      IF (KRNGE.LE.JRGEB(I)) GO TO 90
      CONTINUE
      8  AA=KRNGE - JRGEE(I-1)
      90  BB=JRGEB(I) - JRGEB(I-1)
      CC=AA/BB
      AA=PHB(I)-PHB(I-1)
      BB=CC*AA
      PHIT=PHB(I-1)+BB
      M=M+1

CCCCC
      COMPUTATION OF EXPECTED DAMAGE PER MOVE GIVEN:RATE OF FIRE,HIT PROB
      ABILITY,SEA STATE,EXPECTED DAMAGE GIVEN A HIT,JAMMING FACTOR,ANGLE
      OF DE TARGET.

      EDMM=FEDHR*PHIT*SRF*SEAST*XJANN*TAGTA
      GO TO 500

CC
      30 IF (KRNGE.LE.R2) GO TO 100
      GO TO 1000
      100 WRITE(6,13)
      13  FORMAT(3X,1 MISSILE ENGAGEMENT')
      14  WRITE(6,14) NS
      14  FORMAT(3X,1 TARGET NAME=,I4)

CCCCC
      COMPUTATION OF TARGET MISSILE DEFENSE CAPABILITIES

```

```

K=0
WRITE(6,15)NM
15 FORMAT(3X,' NUMBER OF INCOMING MISSILES DETECTED=',I4)
PK1M=.7
PK2M=.25
CALL SRND(IX1,ZZ,N,1,0)
RT1(I)=ZZ
SDC(I)=DIFAC*RT1(I)
IF(SDC(I).LE.PK1M)AND. SDC(I).GT.PK2M) GO TO 110
IF(SDC(I).LE.PK2M) GO TO 120
110 K=K+1
WRITE(6,16)K
16 FORMAT(3X,' INCOMING MISSILE SHUTDOWN=',I4)
120 K=K+1
WRITE(6,17)K
17 FORMAT(3X,' INCOMING MISSILE SHUTDOWN=',I4)
GO TO 130
130 HALIVE=NM-K
WRITE(6,18)HALIVE
18 FORMAT(3X,' NUMBER OF MISSILES ALIVE=',I4)
GO TO 1000
140 IMPAT=0
DO 5 I=1,HALIVE
CALL SRND(IX2,YZ,N,1,0)
RT2(I)=YZ
IF(RT2(I).GT. ZPHIT) GO TO 5
IMPAT=IMPAT+1
5 CONTINUE
IF(IMPAT.GT.0) GO TO 150
IMPAT=0
150 WRITE(6,19)IMPAT
19 FORMAT(3X,' NUMBER OF IMPACTS ON TARGET=',I4)

CCCCC
COMPUTATION OF EXPECTED DAMAGE AS FUNCTION OF TARGET SIZE

DO 6 I=1,21
IP(TONS.LE.DISP(I)) GO TO 160
6 CONTINUE
T=TONS-DISP(I-1)
Q=DISP(I) - DISP(I-1)
P=T/Q
T=EDMH(I) - EDMH(I-1)
Q=PAT
EXPH=EDMH(I-1)+Q

```

FAK01430
 FAK01440
 FAK01450
 FAK01460
 FAK01470
 FAK01480
 FAK01490
 FAK01500
 FAK01510
 FAK01520
 FAK01530
 FAK01540
 FAK01550
 FAK01560
 FAK01570
 FAK01580
 FAK01590
 FAK01600
 FAK01610
 FAK01620
 FAK01630
 FAK01640
 FAK01650
 FAK01660
 FAK01670
 FAK01680
 FAK01690
 FAK01700
 FAK01710
 FAK01720
 FAK01730
 FAK01740
 FAK01750
 FAK01760
 FAK01770
 FAK01780
 FAK01790
 FAK01800
 FAK01810
 FAK01820
 FAK01830
 FAK01840
 FAK01850
 FAK01860
 FAK01870
 FAK01880
 FAK01890
 FAK01900

```

PHIT=EXPM
COMPUTATION OF KILL PROBABILITIES AS A FUNCTION OF RANGE
DO 7 I=1,21
  IF (KRNGE.LE. TAR(I)) GO TO 170
  CONTINUE
  TT=KRNGE- TAR(I-1)
  QQ=TAR(I) -TAR(I-1)
  PP=TT/ QQ
  TT=VHIT(I) -YHIT (I-1)
  QQ=PP*TT
  EHHIT=YHIT(I-1) +QQ
  PEDHR=EHHIT
170
COMPUTATION OF DAMAGE PER MOVE AS A FCN OF EXPECTED DAMAGE PER
NUMBER OF MISSILE IMPACTS, WARHEAD JAMMING FACTOR,KILL PROBABILITY
WHEAD=HWEIT/250
TAGTA=1.
EDHM=EHHIT*PHIT*IMPAT*YJAMH*WHEAD*TAGTA*SEAST
PEDHR=EHHIT
COMPUTATION OF WEAPONS COVERAGE AREA ON THE TARGET
500 SBAND=EDHM*TBARLE
COMPUTATION OF REMAINING TARGET LIFE AFTER EACH MOVE
SUM=EDMM+SUM
RLIFE=SLIFE(1-( SUM))
COMPUTATION OF CUMMULATIVE DAMAGE
CDMPO=SLIFE-RLIFE
TARGET FLOATING CAPABILITIES AFTER EACH MOVE
FLCAP=(1-(CDMPO/SLIFE))100
IF (FLCAP.GT.0.) GO TO 190
GO TO 999
GENERATION OF UNIFORM RANDOM DEVIATES IN ORDER TO ASSET LOCATION OF
WEAPON IMPACT UPON THE TARGET.
190 CALL LRND(IX3,YY,N,1,0)

```

PAK02390
PAK02400
PAK02410
PAK02420
PAK02430
PAK02440
PAK02450
PAK02460
PAK02470
PAK02480
PAK02490
PAK02500
PAK02510
PAK02520
PAK02530
PAK02540
PAK02550
PAK02560
PAK02570
PAK02580
PAK02590
PAK02600
PAK02610
PAK02620
PAK02630
PAK02640
PAK02650
PAK02660
PAK02670
PAK02680
PAK02690
PAK02700
PAK02710
PAK02720
PAK02730
PAK02740
PAK02750
PAK02760
PAK02770
PAK02780
PAK02790
PAK02800
PAK02810
PAK02820
PAK02830
PAK02840
PAK02850
PAK02860

HPLACE=500*YY
DETERMINATION OF THE TARGET ELEMENTS WHICH WERE HIT OR ARE LOCATED
WHITIN IMPACT AREA.

HALP=SBAND/2
UHALP=HPLACE+HALP
THALP=HPLACE-HALP

CALCULATIONS OF SENSORS KILL- NOT- KILL DAMAGE FOR AIR RADAR
SURFACE RADAR, ECM, ECCM, AND DAMAGE FOR HELO ON BOARD.

HLPK=.8
PCPK=.7
SRPK=.5
ARPK=.4
ACPK=.2
CALL LRND (IX4,X,N,1,0)
SES=YYY
IF {SES .GT. AND.SES .LE. ACPK} GO TO 51
IF {SES .GT. ACPK .AND. SES .LE. ARPK} GO TO 61
IF {SES .GT. ARPK .AND. SES .LE. SRPK} GO TO 71
IF {SES .GT. SRPK .AND. SES .LE. PCPK} GO TO 81
IF {SES .GT. PCPK .AND. SES .LE. HLPK} GO TO 91
IF {SES .GT. HLPK} GO TO 999

51 GO TO 999
61 WRITE(6,32)
71 GO TO 999
81 WRITE(6,33)
91 GO TO 999
999 J=22

DETERMINATION OF DAMAGE DEGRADATION OF TARGET ELEMENTS BY TAKING
IN CONSIDERATION THEIR INDIVIDUALS DAMAGE FACTORS.

WRITE(6,22) DAMAGE RESUHEN
22 FORMAT(3X,1) PEDHR,EDHM,BLIFE,CDMPO,FLCAP,SLIFE,PHIT,HPLACE,XJAMM,
SBAND
WRITE(6,24)

```

24 FORMAT(//,5X,' TARGET ELEMENTS WHICH WERE DAMAGE DURING THE MOVE
      WRITE(6,25)
25 FORMAT(5X,' TARIDENT',5X 'TARPLACE',5X,' TARCOND',)
      DO 10 I=1,J
      IP(TPLACE(NS,I)).LT.THALF.OR. TPLACE(NS,I).GT. UHALF) GO TO 10
      GO TO 210
210 TCOND(NS,I)=TCOND(NS,I) - TEFAC(NS,I)*TCOND(NS,I)
      IF(TCOND(NS,I).LT.0.) TCOND(NS,I)=0.
      WRITE(6,26) IDENT(NS,I),TPLACE(NS,I),TCOND(NS,I)
10 CONTINUE
      WRITE(6,27)
      WRITE(6,28)
27 FORMAT(//,5X,' SURVIVAL CONDITION OF ALL TARGET ELEMENTS AFTER MOVE
      E.
28 FORMAT(5X,' TARIDENT',5X 'TARCONDE',5X 'TARFACTOR',5X 'TARPLACE',)
      WRITE(6,29) (IDENT(NS,I),TCOND(NS,I),TEFAC(NS,I),TPLACE(NS,I),I=1
      J)
29 FORMAT(3X,' RANGE BIGGER THAN DETECTION RANGE')
12 FORMAT(3X,' TARGET ASPECT=',F8.3)
29 FORMAT(//,6X,I4,9X,F8.1,4X,F8.3,4X,F8.1,/)
29 FORMAT(//,6X,I4,9X,F8.1,7X,F8.2,/)
23 FORMAT(3X,' EXPECTED DAMAGE HIT=',F8.3,/,4X,' EXPECTED DNAGE PER
      MOVE',F8.3,/,CAP=',F8.3,/,HIT PROBAB
      4X,F8.3,/,FLYING CAP=',F8.3,/,JAMMING FACTOR=',F8.3
      3X,' COVER AGE FACTOR=',F8.3,/)
31 FORMAT(3X,' ACTIVE COUNTERMEASURES CAPABILITIES LOST')
32 FORMAT(3X,' AIR DETECTION CAPABILITIES LOST')
33 FORMAT(3X,' SURFACE DETECTION CAPABILITIES LOST')
34 FORMAT(3X,' PASSIVE COUNTERMEASURES CAPABILITIES LOST')
35 FORMAT(3X,' HELICOPTER DESTROYED')
      GTIME=GTIME+3
      WRITE(6,206)
C1000 FORMAT(3X,' NO AIRBORNE MISSILE AT THE MOMENT')
C 206
1000 WRITE(4,DATA2)
      STOP
      END
      FAKO2870
      FAKO2880
      FAKO2890
      FAKO2900
      FAKO2910
      FAKO2920
      FAKO2930
      FAKO2940
      FAKO2950
      FAKO2960
      FAKO2970
      FAKO2980
      FAKO2990
      FAKO3000
      FAKO3010
      FAKO3020
      FAKO3030
      FAKO3040
      FAKO3050
      FAKO3060
      FAKO3070
      FAKO3080
      FAKO3090
      FAKO3100
      FAKO3110
      FAKO3120
      FAKO3130
      FAKO3140
      FAKO3150
      FAKO3160
      FAKO3170
      FAKO3180
      FAKO3190
      FAKO3200
      FAKO3210
      FAKO3220
      FAKO3230
      FAKO324
      FAKO33a

```

CC BLUE DATA ONE

```

C&DATA 1
NS=4
KRRNGE=39678.
TARBLE=500.
TARWI=55.
TONS=5643.

```


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